

REZNIKOV, N.I., ~~na~~aluzhennyi deyatel' nauki i tekhniki RSFSR doktor
tekhn.nauk, prof.; MITRYAYEV, K.F., kand.tekhn.nauk

All-Union scientific and technical conference of institutions
of higher learning on the machinability of heat-resistant
and titanium alloys. Vest.mashinostr. 43 no.2:90-91 F '63.
(MIRA 16:3)

(Metal cutting)

MITRYAYEV, K.F., kand.tekhn.nauk; KOMISSAROV, V.I., inzh.

Investigating cutting temperature conditions in face milling of
heat-resistant and titanium alloys. Izv.vys.ucheb.zav.; mashinostr.
no.6:190-199 '63. (MIRA 16:10)

1. Kuybyshevskiy aviatsionnyy institut.

Butt-milling of titanium alloys

8/122/62/000/000/003/003
A006/A101

best material is BK6M (VK6M) sintered carbide. Optimum grinding angles of the cutter are $\gamma = 5 \div 7^\circ$; $\lambda = 5 \div 10^\circ$; $\alpha = 10 \div 15^\circ$. For cutting VT6 and OT4 alloys with VK6M cutters, the following conditions are recommended: $v = 40 - 60$ m/min.

$s_z = 0.05 - 0.15$ mm/tooth, at a displacement of the mill $\frac{k}{D} = 0.05 \div 0.1$. At the initial stage of cutting, when the cutter is incised into the work piece, the cutting speed should be reduced by about twice in comparison to the speed during the established process. There are 7 figures and 1 table.

3/122/62/000/000/000/000
A006/A101

AUTHORS: Komissarov, V. I., Engineer, Mitryayev, K.F., Candidate of Technical Sciences

TITLE: Butt-milling of titanium alloys

PERIODICAL: Vestnik mashinostroyeniya, no. 9, 1962, 68 - 70

TEXT: Information is given on results of investigation the suitability of BT 6 (VT6) and OT4 (OT4) titanium alloys for butt milling. The investigation was carried out under the supervision of Professor N. I. Reznikov, Doctor of Technical Sciences at the cutting laboratory of the Kuybyshevskiy aviatsionnyy institut (Kuybyshev Aviation Institute). The tests were made on a horizontal "Ervag" milling machine. A 130 mm diameter cutter was used with blades having sintered carbide or high speed steel plates. The most suitable alloy for the blades was determined by asymmetrical milling of VT6 alloy; the cutter was adjusted in respect to the work piece by a displacement $k = 6 \text{ mm} \left(\frac{k}{D} = 0.045 \right)$. The tests show that butt milling of titanium alloys VT6 and OT4 with sintered carbides is more efficient than milling with high-speed steel blades (P9K5 (R9K5) and P9K10 (R9K10)). In this case the

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New investigations in the dynamics and thermal ... S/792/62/000/000/004/004

The actual maximums are perhaps 20-25% higher than the recorded maximum means. The single-tooth method provides T readings that not only are closer to the true values, but also permit the thermal-load determination for each individual tooth. The thermal loads on the cutter teeth are not uniform. On several teeth located in the central portion of the lead-in zone, the maximal T's attain 500-600°C even during normal cutting; the use of an effective cooling medium and frequent axial shifts of the milling cutter is of much significance. Good equalization of the thermal load between the individual teeth of a cutter or the application of high-temperature-resistant materials in milling cutters permits a significant increase in the productivity of milling heads through increases in either cutting speed or feed. There are 18 figures, 2 tables, and 7 Russian-language Soviet references. //

ASSOCIATION: None given.

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New investigations in the dynamics and thermal ... S/792/62/000/000/004/004

with a single tooth-billet hump. Individual oscillograms are shown, also a log-log graph of the mean torque versus feed per revolution, from which a power expression similar to that existing for free cutting can be derived. A correction factor for various steels (function of the necking and the tensile strength) is derived. Similar expressions and correction coefficients are found for both the mean and the maximal torque, the mean peripheral cutting force, and the effective power as functions of the module, the feed, the cutting speed, the number of teeth of the gear being cut (this is a subject of considerable debate between various Soviet authors), the milling-cutter wear, and the depth of milling. A comprehensive formula including all of these correction factors is developed for each of the four milling-process parameters M_{av} , M_{max} , $P_{peripheral}$, and N_{eff} . The single-tooth-cutting investigation afforded means for the experimental study of the load distribution between the separate teeth of a worm-type cutter as a function of the various milling-process parameters. It was established that most of the load devolves on a small group of teeth (5 to 8) located in the central portion of the lead-in zone and that the load on those teeth is 2 to 3 times as high as the mean-load level of all cutting teeth. Investigation of the cutting temperature: The single-tooth-cutting procedure affords a more dependable temperature measurement than the multiple-tooth-cutting procedure, since the so-called maximum temperatures measured in a multi-tooth cutting are no more than maximum means of several cutting elements engaged in different stages of cutting.

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S/792/62/000/000/004/004

AUTHOR: Mitryayev, K. F., Engineer.
TITLE: New investigations in the dynamics and thermal phenomenology of gear-tooth milling.
SOURCE: Progressivnyye metody proizvodstva zubchatykh koles i ikh tekhnologichnost'. Mosk. gor. nauchno-tekhn. obshch-vo mashinostr. prom. Moscow, Mashgiz, 1962, 286-302.

TEXT: The paper describes a new low-inertia electroinductive torquemeter designed by the author and Dotsent B. A. Kravchenko for a range of up to 40 kg·m and adapted to use in the model-532 gear millers (module 1 to 6); the tests were performed at the Kuybyshev Aviation Institute under the direction of Prof. N. I. Reznikov. The dynamometer consists of a circular rim and a hub mutually connected by a set of thin, elastic, spokes. Two inductive sensors, with a gap that is altered by any torsional rim-versus-hub deformation, form part of two of the arms of an unbalanced a.c. bridge (carrier f 2000 cps). Any resulting e.m.f. is amplified and is registered on film via an MHO-2 (MPO-2) loop oscillograph. Investigation of the effects of various factors on the mean and maximal torque: Both multi-tooth (ordinary) and single-tooth cutting was done. In multi-tooth cutting the mean torque, the maximum torque for each rack of teeth, and the arithmetic-mean maximum torque for each rack were recorded. Single-tooth cutting was done on special billets

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S/122/61/000/002/006/011
A161/A126

AUTHORS: Mitryayev, K. F., Candidate of Technical Sciences, Komissarov,
V. I., Engineer

TITLE: End milling of EI643 high-strength steel

PERIODICAL: Vestnik mashinostroyeniya, no. 2, 1961, 55 - 58

TEXT: The article presents the results of an experimental investigation of the machinability of EI643 (EI643) steel carried out by the authors under supervision of Professor Doctor of Technical Sciences N. I. Reznikov. EI643 steel is a special grade used for critical power machine parts. [Abstracter's note: The steel composition is not given]. Its properties make this steel difficult to cut, and particularly by end milling. Experimental milling has been done on an "Ervag" ("Ervag") horizontal milling machine, with a standard (ГОСТ 8529-57/ГОСТ 8529-57) end mill 130 mm in diameter, with one or two blades tipped with T15K6 (T15K6) and T30K4 (T30K4) alloy, without coolant. T15K6 alloy tips proved to be better; they withstood about 100 min. cutting, compared to only 30 min with T30K4 tips. There are 7 figures, 1 table and 2 Soviet-bloc references.

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Investigating the cutting temperature ...

S/123/61/000/014/024/045
A004/A101

and determine the number of its axial displacements. 4) To increase the productivity of gear milling it is recommended to raise the feed up to 5 mm/rev at cutting speeds in the range of 25 - 35 m/min and good cooling. At feeds of 6 - 12 mm/rev and cutting speeds of more than 440 m/min it is necessary to equalize the thermal load of the teeth. There are 7 figures and 5 references.

[Abstracter's note: Complete translation]

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S/123/61/000/014/024/045
A004/A101

AUTHOR: Mitryayev, K.F.

TITLE: Investigating the cutting temperature during gear milling

PERIODICAL: Referativnyy zhurnal. Mashinostroyeniye, no. 14, 1961, 67, abstract 14B460 ("Tr. Kuybyshevsk aviats. in-t", 1960, no. 9, 51 - 63)

TEXT: The author describes a method of investigating the temperature during gear milling for single-tooth and aggregate milling. The cutting temperature is measured with the aid of natural thermocouples, the blank being insulated from the machine tool. The temperature readings were recorded on a cinefilm with the aid of the МПО-2 (MPO-2) loop oscillograph. The following facts were established as a result of the investigations: 1) The results of temperature investigations are the most significative for single-tooth milling. 2) The milling cutter teeth do not warm up uniformly. During normal milling conditions the temperature of the cutter middle teeth attains 500 - 600°C. It is recommended to use effective coolants and axial displacement of the milling cutter. 3) The obtained formulae make it possible to set the milling cutter more exactly

Card 1/2

MITRIN, V.P., Mech Tech Sci --(disc) "Study of the process
of gear-cutting with a balling machine." Kiev, 1954. 13 pp
with drawings. (Min of Higher Education USSR. Director of
Lenin Polytech Inst), 100 copies (51,30-53,100)

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SOV/123-59-16-64878

Electroinductive Dynamometer for the Measurement of the Stresses at the Gear Cutting Process

the cutting stress the spokes are bent, the rim is displaced relative to the hub, which leads to an increase of the mentioned clearance in one pick-up and to a decrease in the other. When the torque at the spindle changes in the range of 0 - 45 kilogrammeter the clearance is changed by 0.1 mm; the changes in inductance of the pick-ups arising from this are recorded by an electric device the connection of which is effected by a current collector. The electric circuit of the device consists of the feed unit, the sound generator of the ZG-10 type, and the amplifier. If a resistance potentiometer is installed in the circuit it is possible to obtain 5 ranges of different sensitiveness. The current at the output of the amplifier, which is the gage for the torque to be measured, is recorded by a loop oscillograph. Examples of operating and gaging oscillograms are stated, and also a gaging graphic of one of the measurement ranges, which shows the linear relation between the torque to be measured and the indication of the oscillograph. Results are given of the investigation of the dynamics of gear cutting on the gear cutting machine "532" with standard single-thread worm cutters of medium module ($m = 1.75 - 5$), steel of R9 grade being used. 3 references.

K.S.M.

Card 2/2

SOV/123-59-16-64878

Translation from: Referativnyy zhurnal. Mashinostroyeniye, 1959, Nr 16, p 170 (USSR)

AUTHORS: Kravchenko, B.A., Mitryayev, K.F.

TITLE: Electroinductive Dynamometer for the Measurement of the Stresses at the Gear Cutting Process

PERIODICAL: Tr. Kuybyshevsk. aviats. in-t, 1958, vyp. 7, 87 - 100

ABSTRACT: For the investigation of the dynamics of gear cutting an inductive torsion dynamometer was used. The elastic part of the dynamometer is of disk-shaped execution, manufactured of 30KhGSA steel; the rim and hub of the disk are connected by 10 radial spokes of rectangular cross-section, subjected to bending. The rim is fastened to the flange of a conic shaft, by the aid of which the dynamometer is adjusted in the spindle of the milling machine. Worm cutters are placed on the mandrel, fastened to the hub. In the interior of the elastic part 2 inductive pick-ups are fitted, the cores of which, assembled of Π -shaped transformer iron, are fastened to the rim while the armatures are fastened to the hub. With 400 turns and an initial clearance of 0.25 - 0.3 mm between armature and core the inductance of the pick-ups amounts to 40 millihenry. Under the effect of

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L 45596-66

ACC NR: AT6014330

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equations for two cylindrical surfaces whose genetrices are parallel to two different coordinate axes. This die is also set by using a standard pipe. The die is mounted in the fixed part of the press where the pipe is bent in two operations. Diagrams are also given for two-plane pipe bending. Both dies are universal and can be used for producing other configurations than those presented. Orig. art. has: 10 figures, 1 formula.

SUB CODE: 13/ SUBM DATE: 12May61

Card 2/2 *ds*

L 45596-66 EMT(l)/EMT(m)/EMP(t)/ETI/EMP(k) IJP(c) JD/HW/JH

ACC NR: AT6014330

SOURCE CODE: UR/2529/62/000/070/0097/0105

AUTHOR: Mitryayev, I. M.

ORG: None

TITLE: Dies for pipe bending

SOURCE: Kazan. Aviatsonnyy institut. Trudy, no. 70, 1962. Aviatsonnaya tekhnologiya i organizatsiya proizvodstva (Aviation engineering and organization of production), 97-105

TOPIC TAGS: die, pipe, metal forming press, bending machine, *METAL BENDING*

ABSTRACT: The author studies dies for bending copper, aluminum, steel and brass pipe of small diameter. The dies are used on hydraulic and pneumatic presses. Pipes are bent with fillers and without fillers depending on their intended use. Dies are considered for bending pipes in single and double planes. Those for bending pipes in a single plane have various center line curvatures. The die is set with a standard pipe and then fixed to the immobile part of the press. The pipe is inserted and bent in one operation. Good production results were achieved without using fillers by covering the male and female die surfaces with sheet rubber. Diagrams are given for the arrangement of the dies and bending configurations. In the case of two-plane pipe bending the die has the form of a space curve. The line in space can be given by

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1. 3051-46
ACC NO. 122026395

From this the velocity of point E is found as

$$V_E = \frac{V_C}{r_C} \cdot r_E$$

and the acceleration as

$$r_E = V \sqrt{r_C^2 + r_E^2}$$

$$a_E = \frac{a_C}{r_C} \cdot r_E$$

Neglecting friction forces, the lifter force P_y is derived as

$$P_y = \frac{P V_E \cos(PV_E)}{V_{23}}$$

for any position of the space mechanism (where V_{23} = velocity of part 2 with respect to 3). Orig. art. has: 46 formulas and 2 figures.

SUB CODE: AC, ME/ SUBM DATE: 05Oct63/ ORIG REF: 001

Cont 4/4

I 8001-46
ACE NR 125126595

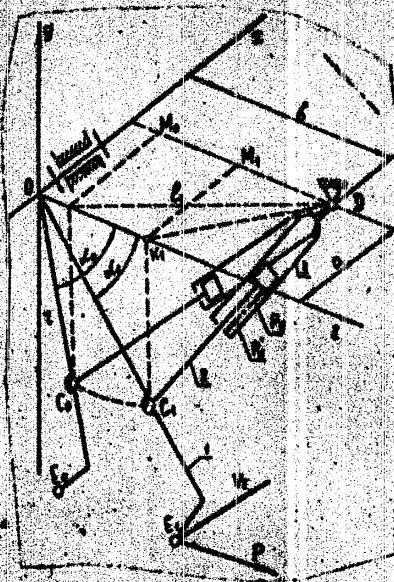


Fig. 2. Space mechanism coordinates

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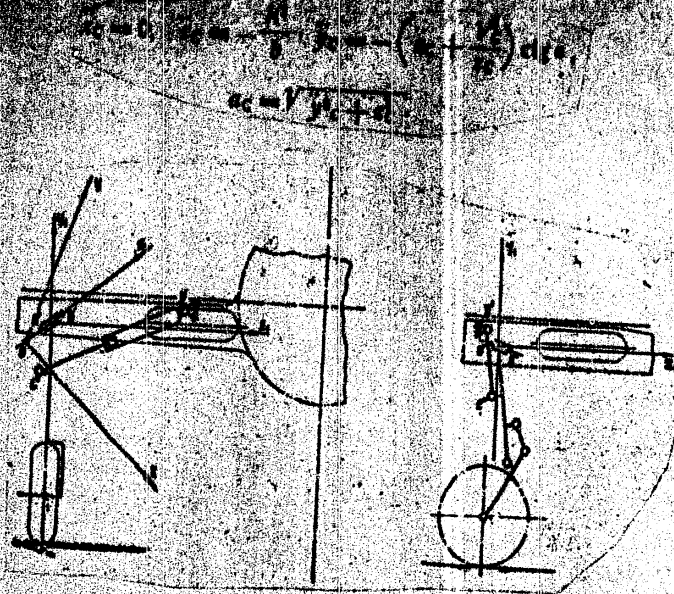


Fig. 1. Space mechanism

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1.5001-46
 ACC NO. 13506595

ORG: Kazan Aviation Institute (Kazanskiy aviatsionnyy institut)

TITLE: Determination of forces in the lifter of a landing gear space mechanism

SOURCE: Kazan. Aviatsonnyy institut. Trudy, no. 81, 1963. Prikladnaya mekhanika (Applied mechanics), 35-44

TOPIC TAGS: space mechanism, solid kinematics, aircraft landing gear, linkage force

ABSTRACT: The kinematics and lifter forces of a space mechanism shown on Fig. 1 (often used to retract aircraft landing gears) are investigated. Equations of the trajectory, velocity, and acceleration of point C in the coordinates shown in Fig. 2 are derived respectively as

$$x_c = 0, \quad z_c = -\frac{K^2 b^2 - 2Kl - 2br \cos \alpha_1}{2b}, \quad y_c = z_c \operatorname{tg} \alpha_1$$

$$x_c = 0, \quad z_c = -\frac{K^2 b^2 - Kl}{b}, \quad y_c = -\frac{z_c}{y_c} z_c$$

$$V_c = \sqrt{y_c^2 + z_c^2}$$

MITRYAYEV, I.M.

Kinematic and force investigation of some types of retractable landing
gears. Trudy KAI no.62:109-119 '61. (MIRA 17:2)

MITRYAYEV, I.M.

Determining the axis of rotation of retractable landing gears. Trudy
KAI 30:153-159 '55. (MIRA 10:6)
(Airplanes--Landing gear)

MITRYAYEV, I.M.

Method of "reversible motion" in the kinematics of plane mechanisms.
Trudy KAI 22:23-30 '49. (MLRA 10:6)
(Mechanical movements)

MITRYAYEV, I. M.

33180. Metod "Obrashcheniya Dvizheniya" V Kinetatike Ploskikh
Mekhanizmov. Trudy Kazansk. Aviats. In-Ta,
XXII, 1949, C. 23-30

SO: Letopis 'Zhurnal'nykh Statey, Vol. 45, Moskva, 1949

APPROVED FOR RELEASE: 06/23/11: CIA-RDP86-00513R001134700007-6

MITRYAYEV, I. M., Engr. Cand. Tech. Sci.

Dissertation: "Spatial Mechanisms of a Landing Gear, Their Classification, Kinematics and Kinetostatics." Moscow Order of Lenin Aviation Inst. Ineni S. Grigorikidze, 25 Dec 77.

SO: Vechernyaya Moskva, Dec, 1947 (Project #17836)

ISKHAKOV, T.G.; MITRYAYEV, I.M.

Arrangement of type bars in the segments of typewriters. Trudy
KAI 72:16-24 '62. (MIRA 16:8)
(Typewriters)

ACCESSION NR: AN4014557

ing surfaces of the male and female dies are covered with sheet rubber. A die for bending of pipes in two planes consists of one female and two male dies: vertical and horizontal. The bending is carried out with two strokes of the press. The first drawing is made by the vertical male die; then the united female and vertical male dies are rotated through 90° and at the second stroke of the press the final bending is accomplished by the horizontal male die. The female die and the male dies consist of a body and plates. Setup of the die is likewise accomplished by a calibration pipe, the female die being set up first and the male dies then being adjusted to the female die. Ill., 10. Ye. Vayner.

DATE ACQ: 09Jan64

SUB CODE: IE, ML

ENCL: 00

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ACCESSION NR: AR4014557

S/0276/63/000/012/V022/V022

SOURCE: RZh. Tekhnologiya mashinostroyeniya, Abs. 12V140

AUTHOR: Mitryayev, I. M.

TITLE: Dies for pipe bending

CITED SOURCE: Tr. Kazansk. aviats. in-ta, vy*p. 70, 1962, 97-105

TOPIC TAGS: pipe bending, pipe bending die, small diameter pipe bending, small pipe bending, pipe bending punch, pipe bending press, punch press

TRANSLATION: A description is given of dies for bending of pipes of small diameter from steel and non-ferrous metals. The male and female die for bending of pipes in one plane consist of a body and a series of parallel plates. Setup of the die is accomplished with the help of a calibration pipe. The plates of the female die are set in the body at a height corresponding to the standard so that the edges of the plates form the necessary profile. The male die is adjusted according to the female die or according to the calibration pipe. In such a die the bending is accomplished at one stroke of the press. The work-

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MITRYASOV, P.P., inzhener.

Diagram of an idle run regulator for a welding transformer.
Elektrichestvo no.5:88 My '54. (MLRA 7:6)

1. Mekhanicheskiy zavod, g. Shchigry Kurskiye.
(Electric transformers)

MITRYASHIN, M.L., inzh.

Technological layouts of sand and gravel plants and crushing and
sorting plants of the United States. Stroi. mat. 7 no.3:35-40 Mr
'61. (MIRA 14:4)

(United States--Sand and gravel plants)
(United States--Stone industry)

MITRYASHIN, M.L., inzh.; TARASOV, Yu.D., inzh.

Automatically controlled sand and gravel plants. Stroi. mat. 5
no.10:8-11 0 '59. (MIRA 13:2)
(Sand and gravel plants) (Automation)

MITRYANIN, P. N.

MITRYANIN, P.N., kandidat sel'skokhozyaystvennykh nauk, dotsent.

Electric power utilization in animal husbandry of collective farms served by the Georgevskaya Machine-Tractor Station of Kuybyshev Province. Izv.TSKhA no.1:165-174 '57. (MIRA 10:7)
(Kuybyshev Province--Electricity in agriculture)

TISHCHENKO, D.V.; KISLITSYN, A.N.; ZAGARMISTR, O.S.; Prinimali uchastiye:
VAPYSHEVA, K.M., mladshiy nauchnyy sotrudnik; MITRYAKOVA, L.Kh.;
SEMEANOVA, A.A., mladshiy nauchnyy sotrudnik

Using phenylic acids of wood tar pitch as raw material for
obtaining viscosity reducers. Sbor.trud.TSNILKHI no.14:46-52 '61.
(MIRA 16:4)

1. Starshiy tekhnik laboratorii drevesnykh smol TSentral'nogo
nauchno-issledovatel'skogo i proyektного instituta lesokhimicheskoy
promyshlennosti (for Mitryakova). 2. Vsesoyuznyy nauchno-
issledovatel'skiy institut burovoy tekhniki (for Semenova).
(Wood tar) (Phenols)
(Chemical tests and reagents)

MITRYAKOV, N.F. (Tyumen', Komsomol'skaya ul. d. 58)

Posttraumatic esophagotracheal fistula. Vest. khir. 90 no. 11: 112-116
N 163. (MIRA 17:113)

1. Iz 2-go khirurgicheskogo otdeleniya (rav. -- N.F.Mitryakov) Tyumenskoy
oblastnoy bol'nitsy (glavnyy vrach -- A.A.Molnyenko).

MITRYAKOV, N.F. (g. Tyumen', Komosomol'skaya yl., d. 58)

Surgical treatment of "sieve lung". Grud.khir. no.4:106-107
Jl-Ag '62. (MIRA 15:10)

1. Iz 2-go khirurgicheskogo otdeleniya (zav. N.F.Mitryakov)
Tyumenskoy oblastnoy bol'nitsy (glavnyy vrach A.A.Moiseyenko).
(LUNGS---DISEASES)

MITRYAKOV, N. F.

Method for treating the bronchus in radical operations on the lungs; (clinical experimental work). Preliminary report. Grud. khir. 4 no.1:74-78 Ja-F '62. (MIRA 15:2)

1. Iz khirurgicheskogo otdeleniya (zav. N. F. Mitryakov) Tyumenskoy oblastnoy bol'nitsy (glavnyy vrach A. A. Moiseyenko).

(LUNGS---SURGERY) (BRONCHI---SURGERY)

MITRYAKOV, N.F.

Case report on a tumor of the thyroid gland. Khirurgiia 37
no.5:126 My '61. (MIRA 14:5)

1. Iz khirurgicheskogo otdeleniya (zav. N.F. Mitryakov)
Tyumenskoy oblastnoy bol'nitsy (glavnyy vrach A.A. Moiseyenko).
(THYROID GLAND--TUMORS)

NITRYAKOV, N.F. (Tyumen', Komsomol'skaya, ul., d. 58)

Spontaneous valvular pneumothorax treated by surgery. Vest.khir.
82 no.1:135 Ja '59. (MIRA 12:2)

1. Iz 2-go khirurgicheskogo otdeleniya (zav. L.Ya. Shnitser)
Tyumenskoy oblastnoy bol'nitsy.
(PNEUMOTHORAX)

On periodic solutions of systems of nonlinear

8/044/63/000/002/023/050
A060/1126

where the α_i are some constants. The following theorem is proved: The system of differential equations (1) admits of a unique system of solutions continuous together with their partial derivatives up to the second order with respect to x and up to the first order with respect to t in the domain D satisfying the conditions (2), periodic in t with period unity if the functions p_i , q_i and f_i satisfy the conditions I and II, and the parameters μ_i are sufficiently small in absolute value.

[Abstractor's note: Complete translation]

6. periodic solutions of systems of nonlinear

are periodic in t with period unity, satisfy the conditions (2) and may be expanded in series in terms of the fundamental functions. II. The functions f_i are continuous with respect to their arguments, satisfy the boundary conditions

and may be represented in the form of series

$$I_1 = \sum_{n=1}^{\infty} P_n \cdot [a_{1n}(t), \dots, a_{mn}(t), a_{nn}(t), \dots] \varphi_n(x).$$

12345678910111213141516171819202122232425262728293031323334353637383940414243444546474849505152535455565758596061626364656667686970717273747576777879808182838485868788899091929394959697989910010110210310410510610710810911011111211311411511611711811912012112212312412512612712812913013113213313413513613713813914014114214314414514614714814915015115215315415515615715815916016116216316416516616716816917017117217317417517617717817918018118218318418518618718818919019119219319419519619719819920020120220320420520620720820921021121221321421521621721821922022122222322422522622722822923023123223323423523623723823924024124224324424524624724824925025125225325425525625725825926026126226326426526626726826927027127227327427527627727827928028128228328428528628728828929029129229329429529629729829930030130230330430530630730830931031131231331431531631731831932032132232332432532632732832933033133233333433533633733833934034134234334434534634734834935035135235335435535635735835936036136236336436536636736836937037137237337437537637737837938038138238338438538638738838939039139239339439539639739839940040140240340440540640740840941041141241341441541641741841942042142242342442542642742842943043143243343443543643743843944044144244344444544644744844945045145245345445545645745845946046146246346446546646746846947047147247347447547647747847948048148248348448548648748848949049149249349449549649749849950050150250350450550650750850951051151251351451551651751851952052152252352452552652752852953053153253353453553653753853954054154254354454554654754854955055155255355455555655755855956056156256356456556656756856957057157257357457557657757857958058158258358458558658758858959059159259359459559659759859960060160260360460560660760860961061161261361461561661761861962062162262362462562662762862963063163263363463563663763863964064164264364464564664764864965065165265365465565665765865966066166266366466566666766866967067167267367467567667767867968068168268368468568668768868969069169269369469569669769869970070170270370470570670770870971071171271371471571671771871972072172272372472572672772872973073173273373473573673773873974074174274374474574674774874975075175275375475575675775875976076176276376476576676776876977077177277377477577677777877978078178278378478578678778878979079179279379479579679779879980080180280380480580680780880981081181281381481581681781881982082182282382482582682782882983083183283383483583683783883984084184284384484584684784884985085185285385485585685785885986086186286386486586686786886987087187287387487587687787887988088188288388488588688788888989089189289389489589689789889990090190290390490590690790890991091191291391491591691791891992092192292392492592692792892993093193293393493593693793893994094194294394494594694794894995095195295395495595695795895996096196296396496596696796896997097197297397497597697797897998098198298398498598698798898999099199299399499599699799899910001001100210031004100510061007100810091010101110121013101410151016101710181019102010211022102310241025102610271028102910301031103210331034103510361037103810391040104110421043104410451046104710481049105010511052105310541055105610571058105910601061106210631064106510661067106810691070107110721073107410751076107710781079108010811082108310841085108610871088108910901091109210931094109510961097109810991100110111021103110411051106110711081109111011111112111311141115111611171118111911201121112211231124112511261127112811291130113111321133113411351136113711381139114011411142114311441145114611471148114911501151115211531154115511561157115811591160116111621163116411651166116711681169117011711172117311741175117611771178117911801181118211831184118511861187118811891190119111921193119411951196119711981199120012011202120312041205120612071208120912101211121212131214121512161217121812191220122112221223122412251226122712281229123012311232123312341235123612371238123912401241124212431244124512461247124812491250125112521253125412551256125712581259126012611262126312641265126612671268126912701271127212731274127512761277127812791280128112821283128412851286128712881289129012911292129312941295129612971298129913001

[Illegible handwritten text]

are twice differentiable with respect to x , and the second partial derivatives with respect to x and y are bounded and satisfy the conditions

$$= \sum_{j=1}^n \frac{1}{2} \left(\|x_j - \bar{x}\|^2 + \|y_j - \bar{y}\|^2 \right)$$

Card 3/4

On periodic solutions of systems of nonlinear

8/044/63/000/002/023/050
A060/1126

$$u(x, t) = \sum_{n=1}^{\infty} a_n(t) \Phi_n(x)$$

where $\{\Phi_n(x)\}$ is an orthonormed system of fundamental functions of the system of equations

$$\frac{d}{dt} \left[p(t) \frac{du}{dx} \right] + \lambda u = 0, \quad p(0) = p(\pi) = 0,$$

corresponding to the eigenvalues $\{\lambda_n\}$. The functions $p_1(x)$ are positive and continuous together with their derivatives of the first and second order. The fundamental functions satisfy the conditions:

$$\left| \Phi_n(t) \right| \leq B, \quad \left| \frac{1}{\sqrt{\lambda_n}} \Phi_n \right| \leq B, \quad \left| \frac{1}{\lambda_n} \Phi_n' \right| \leq B,$$

where B is a constant. The functions Φ_1 and Φ_2 satisfy the following conditions:

1. The functions Φ_1 are continuous together with their partial derivatives

$\frac{\partial \Phi_1}{\partial x}$ in the domain

$$D = \{0 < x < \pi, 0 < t < 1\}$$

Card 2/3

8/044/63/000/002/023/090
K.60/A126

AUTHOR: Mitropol, A.P.

TITLE: On periodic solutions of systems of nonlinear equations of the parabolic type

ABSTRACT: Referativnyi zhurnal, Matematika, no. 2, 1963, 19, abstract 28219 (Tr. Semakondsk. un-ta, 1962, no. 119, 109 - 114)

TEXT: The author considers the system of equations

$$\frac{\partial u_i}{\partial t} - \Delta u_i = f_i(t, x, u) + p_i(t, x, u), \quad (1)$$

(i = 1, 2, ..., n).

where $p_i(t, x) = \frac{\partial u_i}{\partial t}$ and seeks a solution satisfying the conditions

$$\begin{aligned} u_i(t, 0) &= u_i(t, 1) = 0 \\ u_i(0, x) &= u_i(1, x) \end{aligned} \quad (2)$$

The solution is required in the form of series

Card 1/4

MITRYAGINA, S. F.

Mitryagina, S. F.

"Investigation of Thebaine." Min Health USSR. Moscow Pharmaceutical Inst.
Moscow, 1955. (Dissertation for the Degree of Candidate in Pharmaceutical
Science)

So: knizhnaya letopis', No. 27, 2 July 1955

SARYCHEVA, I.K.; SEREBRENNIKOVA, G.A.; MITRUSHKINA, L.I.; PREOBRAZHENSKIY,
N.A.

New synthesis of 1,2,4-trimethyl-3,6-hydroquinone. Zhur.ob.khim.
31 no.7:2190-2192 J1 '61. (MIRA 14:7)

1. Moskovskiy institut tonkoy khimicheskoy tekhnologii imeni
M.V. Lomonosova.

(Hydroquinone)

MITRUSHIN, M. M.

Drilling and Boring Machinery

Drilling dynamometer of simple construction, Stan. 1 instr. 23 no. 3:37 mr '52.

Monthly List of Russian Accessions, Library of Congress, July 1952. Unclassified.

AUTHOR: Mitrushi, Il'ya

26-58-6-25/56

TITLE: The Forests of Albania (Lesa Albanii)

PERIODICAL: Priroda, 1958, Nr 6, p 93-95 (USSR)

ABSTRACT: Albania is mainly a mountainous country, 47 % of which is covered by forests. The total forestal area amounts to 1.36 million ha. The mean annual temperature varies between 14.5 and 18° C, and the climate is one of the dampest in all of Europe. For that reason the variety of trees growing in Albania is very rich. A list of these trees is given. There are 3 photos.

ASSOCIATION: Institut nauk, Tirana (Albaniya)
(Institute of Sciences, Tirana - Albania)

Card 1/1 1. Geography-Albania 2. Forestry

DEMIRI, Mustafa; MITRUSHI, Il'ya.

Flora and fauna of Albania. Priroda 45 no.8:71-80 Ag '56.
(MLRA 9:9)

(Albania--Botany) (Albania--Zoology)

MITRUSHENKO, I., Geroy Sotsialisticheskogo Truda

Vital necessity. Mast. ugl. 9 no.9:8 S'60. (MIRA 13:10)

1. Nachal'nik uchastka shakhty No.45 kombinata Chelyabinskugol'.
(Coal mines and mining)

BIALECKI, Stanislaw; MITROZEWSKA, Honorata; LITYNSKA, Jadwiga; JEDRZEJEWSKA,
Halina

Complication of intra-articular unions in fractures of the knee and
ankle joints. Chir.narz.ruchu ortop. polska 27 no.1:49-53 '62.

1. Z Kliniki Ortopedycznej AM w Warszawie Kierownik: prof. dr
A.Gruca.
(KNEE fract & disloc) (ANKLE fract & disloc)

KAZHAL, N.; BABA, K.; BOYERU, V.; MITROYU, O.

Diagnosis of virus epidemic hepatitis by means of determining
the activity of the serum aldolase. Zdravookhranenie 3 no.2:
19-23 Mr-Ap '60. (MIRA 13:7)

1. Iz instituta virusologii Akademii nauk Rumynskoy Narodnoy
Respubliki (direktor - akademik, prof. doktor Sht.Sht. Nikolau).
(HEPATITIS, INFECTIOUS) (ALDOLASE)

MITROWSKA, N.

1
The preparation of sulfones of the phenothiazine group.
D. Simer and N. Mitrowska. *Compt. rend. acad. bulgare*
sci. 11, 485-8 (1958) (in Russian) (German summary).
A new method for the conversion of sulfoxides of the pheno-
thiazine group to the sulfones was described. The reagent
used was H_2O_2 in dioxane. The following conversions were
carried out: phenothiazine oxide to phenothiazine dioxide
(yield 87%); phenothiazine to phenothiazine dioxide
(yield 80%); 2,7-dichlorophenothiazine oxide to 2,7-
dichlorophenothiazine dioxide (yield 89%).

M. J. Newlands

3
4E3L
29.9 (WB)

CTK

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99

L 31113-66

ACC NR: AT6008954

bushings are studied. The bushing design shown in Fig. 1 was found to have the best qualities. The supporting strength of caprone bushings is fairly high. Orig. art. has: 2 tables, 2 diagrams, and 1 graph.

SUB CODE: 11/ SUBM DATE: 31Jul65/ ORIG REF: 005

Card 3/3

90

L 31113-66

ACC NR: AT6008954

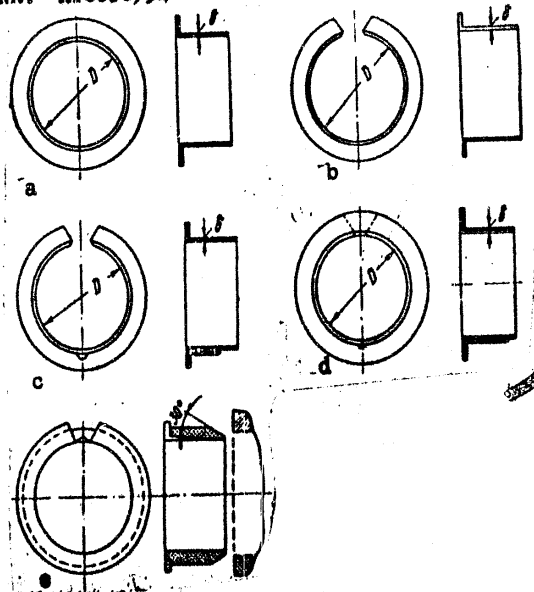


Fig. 1. Designs of tested bushings: a - one-piece thick-walled bushing; b - slotted bushing with oil intake attached to recess with epoxy resin; c - slotted bushing with oil intake attached mechanically; d and e - one-piece thick-walled bushings pressed into recess.

L 31113-66 EWT(m)/EWP(J)/T/ETC(m)-6 LJP(c) VW/DJ/GS/DM
 ACC NR: AT6008954 (A) SOURCE CODE: UR/0000/65/000/000/0149/0155

AUTHOR: Mitrovich, V. P.

ORG: none

TITLE: A study of caprone bushings // ✓

SOURCE: Moscow. Institut mashinovedeniya. Plastmassy v podshipnikakh skol'zheniya; issledovaniya, opyt primeneniya (Plastics in friction bearings; research and experiment in application). Moscow, Izd-vo Nauka, 1965, 149-155

TOPIC TAGS: friction coefficient, wear resistance, lubricant, resin, lubricating oil

ABSTRACT: The advantages and disadvantages of certain designs of thick-walled bushings are discussed (see Fig. 1). The effect of the shaft surface finish on caprone wear is studied. Ground rollers were heat-treated to a hardness of HRC - 38--42. The slip speed was 0.5 m/sec, and the pressure was 110 kg/cm². It is found that the form of the roughness peaks and not the class of smoothness has the deciding influence in caprone wear. Ground rollers with a surface smoothness of ▽ 7 caused the greatest wear. The limiting operating conditions for caprone

Card 1/3

ILLEGIBLE

ACCESSION NR: AP4043329

able aging. Concerning the relationship between abrasion rate and temperature, Kapron showed the best results. Frictional tests on the same machine were carried out at loads of 5 and 38 kg/cm², and a shear rate of 0.22 m/sec. The temperature was increased from room temperature to the melting point of the polymers at a rate of 67-70C per hours, and "oil 12" was added at a rate of 6 drops per minute. Polypropylene had the lowest coefficient of friction, followed by polyformaldehyde. The highest coefficient of friction was found for polyamides, which increased with increasing temperature. At 38 kg/cm², the coefficient of friction of polyformaldehyde and polypropylene decreased with increasing temperature, while that of polyamides increased, although slightly. Orig. art. has: 4 figures.

ASSOCIATION: None

SUBMITTED: 00

ENCL: 00

SUB CODE: OC, MT

NO REF SOV: 004

OTHER: 000

Card

2/2

ACCESSION NR: AP4043329

S/0191/64/000/008/0063/0064

AUTHOR: Mitrovich, V. P.

TITLE: Investigation of the friction and abrasion of some polymers

SOURCE: Plasticheskiye massy*, no. 8, 1964, 63-64

TOPIC TAGS: polymer, friction, abrasion, polypropylene, polyformaldehyde, heat stability, anid, nylon, enant, lubricant, plastic machine part, friction coefficient, polymer wear resistance, Kapron, polyamide

ABSTRACT: The serviceability of polymers used in combination with steel when lubricated with mineral oil under conditions close to those of the operation of bearings, when the frictional unit is liable to become overheated, was investigated in experiments with polypropylene ($\eta = 3.67$, 3.3% low-molecular weight compounds), polyformaldehyde ($\eta = 1.3$ heat-stability constant $K = 0.16$), "anid" (nylon, $\eta = 0.73$) and "enant" ($\eta = 0.75$), using the Kh2-M^2 machine and a unit consisting of a plastic bushing and a 45 HRC steel shaft at a load of 110 kg/cm^2 , shear rate = 0.87 m/sec . The lubricant used was "commercial oil 12" and the unit was run for 6-7 hours at temperatures of 20, 80, 120, and 160°C . The least abrasion was noted with polyamides such as Kapron, enant, anid and AK/7. A temperature increase up to 80°C did not affect their abrasion, but a further increase resulted in consider-

Card 1/2

AM0033662

BOOK EXPLOITATION

S/

Mitrovich, Vadim Petrovich

Study of friction of polyamides on steel (Issledovaniye treniya poliamidov po stali) Moscow, Izd-vo AN SSSR, 63. 0094 p. illus., biblio. Errata printed on inside of back cover. 1,500 copies printed. (At head of title: Akademiya nauk SSSR. Gosudarstvennyy komitet po mashinostroyeniyu pri Gosplane SSSR. Institut mashinovedeniya)

TOPIC TAGS: polyamide, polyamide bearing material, polymer bearing material, kapron, nylon, machine tool bearings

PURPOSE AND COVERAGE: The book contains the principal results of laboratory tests, carried out at the Wear-endurance Laboratory of the Institute of Machine Science and in the Experimental Scientific Research Institute of Metal-Cutting Tools, on plastics with good antifriction properties, primarily the polyamide group. The factors which determine the limiting conditions under which polyamides can operate in friction against steel are examined, and bearings made of kapron were tested for use in mechanisms of metal cutting machinery.

TABLE OF CONTENTS [abridged]:

Card: ~~22~~

MITROVICH, V.P.; FOMICHEVA, M.K.

Method of craters and impressions applied to the study of wear. Zav.
lab. 29 no.2:217-218 '63. (MIRA 16:5)

1. Eksperimental'nyy nauchno-issledovatel'skiy institut
metallorazhushchikh stankov.
(Mechanical wear)

MITROVICH, V.P.

Using capron in manufacturing bearings for the IK62 machine tool.
Stan.i instr. 33 no.6:29-31 Je '62. (MIRA 15:7)
(Plastic bearings)

MITROVICH, V.P., inzh.

Effect of heat treatment on the hardness and certain antifriction
properties of polyamides. Vest.mash. 41 no.3:42-45 Mr '61.

(Plastics--Testing)

(MIRA 14:3)

33011

S/663/61/000/000/000/000
D040/D112

Some aspects of the ...

temperature on the two types of plastics may be due to the increasing specific adhesion in the hot material and not to the increased area of actual contact. The adhesion theory of Bowden and Tabor was confirmed by shear tests. Conclusions: (1) In dry friction of polyamides, and particularly upon an increase in temperature, the friction force depends mainly on the molecular interaction of the friction surfaces; (2) The friction behavior of the studied polymers and the explanation of the variation of the friction factor with temperature is closely connected with the chemical texture of the polymers; (3) It has been revealed that the specific friction force increases with rising temperature in the case of friction of polyamides with steel. There are 6 figures, 1 table and 5 references: 3 Soviet and 2 non-Soviet-bloc. The two references to English-language publications read as follows: R.F. King, D. Tabor. The Effect of Temperature on the Mechanical Properties and the Friction of Plastics. Proc. Phys. Soc., 66, P. 9 (405 B), 1953; F.P. Bowden, D. Tabor. The Friction and Lubrication of Solids. Oxford, 1954.

Card 3/3

33011

S/663/61/000/000/000/000
DO40/D112

Some aspects of the ...

(b) Polyethylene and polytetrafluoro-ethylene whose simplified formulas are:

- ($\text{CH}_2 - \text{CH}_2$) polyethylene;
- ($\text{CF}_2 - \text{CF}_2$) polytetrafluoro-ethylene.

All specimens were products of industrial fabrication. The test machine and devices, and the heating system for the specimens were the same as in the previous experiments (Ref. 1). The tests were conducted with a 1 kg load and a 13.2 m/min sliding velocity. The Super-Rockwell hardness tester used for the hardness measurements at increased temperatures was fitted with a heating arrangement for the indenter; the specimens themselves were heated by an electric heater in the specimen table. The friction factor of the polyamides (which contain polar peptide groups producing considerable cohesion and adhesion forces) rose much more sharply than that of polyethylene or polytetrafluoro-ethylene (which has the lowest adhesive capacity of all existing polymers). As it was also found that the hardness of polyethylene and polytetrafluoro-ethylene decreased more than that of polyamides upon an increase in temperature, it was supposed that the different effect of the

Card 2/3

15.8360 2209

33011

S/663/61/000/000/003/000
D040/D112

AUTHOR: Mitrovich, V.P.

TITLE: Some aspects of the friction behavior of polyamides

SOURCE: Plastmassy kak antifriktsionnyye materialy. Inst. mashinoved.
AN SSSR. Moscow, Izd-vo AN SSSR, 1961, 53-59

TEXT: This article describes experiments made to explain the abrupt increase of the friction factor of polyamides in dry friction with steel upon an increase in temperature. This phenomenon had been observed in previous experiments (Ref 1: V.P. Mitrovich, the preceding article in this symposium, pp 43-52). The present article also contains a description of tests for hardness and shear resistance at increased temperatures. The following materials were chosen for the study: (a) The three most extensively used polyamides whose formulas in simplified form are:

$-\text{[NH(CH}_2\text{)}_5\text{CO]}_n-$	caprone
$-\text{[NH(CH}_2\text{)}_6\text{NHCO(CH}_2\text{)}_4\text{CO]}_n-$	AK7 (AK7) (in the basic mass);
$-\text{[NH(CH}_2\text{)}_6\text{NHCO(CH}_2\text{)}_8\text{CO]}_n-$	П 68 (P68);

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33010

S/663/61/000/000/004/009
D040/D112

Laboratory test data on ...

heating and cooling, and the critical pressure-velocity (pv) value could be increased more than tenfold without any destructive effect: this may be the explanation for the difference in data obtained by different investigators. The plastic specimen blanks were supplied by the laboratory no. 10 (Laboratory no. 10) of NIIPlastmass. Conclusions: The data prove that the friction surface temperature of polyamides in contact with steel under dry-friction conditions has a decisive effect on the friction factor, the intensity of wear, the critical (pv) value, as well as on the nature of the dependences of wear on load and friction factor on sliding velocity. There are 14 figures and 8 references: 4 Soviet and 4 non-Soviet-bloc. The 4 references to English-language publications read as follows: A. Schallamach. Abrasion Pattern on Rubber. Trans. Inst. Rubber Industry, vol. 29, N. 5, 1952; W. C. Milz, L. B. Sargent. Frictional Characteristics of Plastics. Lubrication Engineering, vol. 11, N. 5, 1955; B. Olofsson. Measurement of Friction Between Single Fibers. Textile Research Journal, vol. 22, N. 7, 1952; A. Schallamach. The velocity and temperature dependence of Rubber Friction. Proc. Phys. Soc., vol. 66, N. 331, B. P. 5, 1953.

Card 3/3

33010

S/663/61/500/550/554/555
DO40/D112

Laboratory test data on ...

load, 3 kg. in this case, the plastic stuck to the steel disc, spread over it, and separated in the form of flakes. A further load increase caused melting, and the plastic surfaces acquired a wavy appearance similar to that of rubber subjected to abrasive wear. Contrary to the data of Pascoe, Tabor, Shooter, Milz, Sargent and other investigators who studied the friction behavior of polyamides at low speeds, when the specimens were not heated to any marked degree, the author found that the friction factor did not drop with increasing load. The effect of temperature on friction was therefore studied, with the use of two systems. In the first system, the steel disc and the specimen were heated by a copper rod, which thrust against the disc and was heated by a tubular electric heater. In the second system the disc was cooled by cooling the copper rod. It was found that the temperature had a great effect on the friction factor: cooling reduced the friction factor and heating raised it. It is supposed that the higher friction factor at low speeds is due to more complete contact between the surfaces; this explanation was also given by Olofsson. The mechanism of the friction of polyamides is considered not comparable with the mechanism of viscous flow, although Schallamach and Bartenev consider this can be done in the case of rubber. The friction factor varied more than 3 times through the effect of

Card 2/3

15 8360

33010

S/663/61/000/000/001/000
D040/D112

AUTHOR: Mitrovich, V.P.

TITLE: Laboratory test data on the dry-friction behavior of polyamides

SOURCE: Plastmassy kak antifriktsionnyye materialy. Incl. and index.
AN SSSR. Moscow, Izd-vo AN SSSR, 1961, 43-52

TEXT: The dry-friction behavior of caprone, AK7 (AK7) and П 60 (P60) plastics was studied, as this matter had not been sufficiently studied. A modified Skoda-Sawin test machine was used, the friction being applied by steel discs. The plastics were subjected to varying loads, sliding speeds and temperatures. The test techniques are described in detail. Wear was measured by an indicator with $1/4$ divisions. Some of the caprone specimens were heat treated by heating to 150°C in "vapor" oil, holding for 4 hours and cooling at a rate of $15-20^{\circ}\text{C/hr}$; this did not affect the texture. The heat-treated caprone was tested at a constant sliding velocity of 13.2 m/min and a $0.5-4.5 \text{ kg.}$ load. Friction heat markedly intensified wear. The friction factor curves of all three plastics were analogous. The wear of heat-treated caprone was uniform and the separating white plastic dust did not stick to the discs when the load was below the critical point, but above the critical

Card 1/3

A New Form of Application of the Skoda-Machine 1/03/11/0226/012/023/036
Machine for Friction- and Wear Tests With 10226/012/023/036
Plastic Materials

of the temperature of the sample, that of polyethylene rises under the same conditions much more slowly (with the exception of the temperature near the diffusion point of the polymer) and that of polytetrafluoroethylene drops under the same conditions with increasing temperature. There are 4 figures and 1 Soviet reference.

ASSOCIATION: Institut mashinovedeniya Akademii nauk SSSR
(Institute of Machine Science of the Academy of Sciences,
USSR)

Card 3/3

A New Form of Application of the Škoda-Savin 3/032/60/026/012/025/036
 Machine for Friction- and Wear Tests With 8020/8056
 Plastic Materials

was 20 mm². It was washed with sulfuric ether. The load was varied from 0.5 to 3.75 kg. The sliding rate was 13.2 m/min. The wear intensity was determined under all conditions at given frictional character. The inflections on all curves are due to a change in the character of friction- and wear, which, in the case of increased load, occurs as a result of the increased temperature of the specimens. For investigating the dependence of the wearability and the coefficient of friction of the polymers upon the conditions of heat transfer and the temperature at laboratory conditions, a number of simple devices was constructed. The simulation of various conditions of heat transfer was brought about by cooling the disk by means of water, or by additional electric heating the sample. By means of the first-mentioned device, capron was tested during friction without lubrication under various conditions of heat transfer (Fig. 4a). The most essential dependence of the coefficient of friction, of the intensity of wear, and the usefulness of capron upon the heat transfer conditions at the place of friction is shown by Fig. 4a. Fig. 4b shows the results obtained by friction tests of polyamides (capron, AK-7 (AK-7) and П-68 (P-68)), polyethylene and polytetrafluoroethylene at increased temperatures. The coefficient of friction of the polyamides rises considerably with an increase

Card 2/3

3/332/31, 325/312/325/336
3020/30-6

AUTHOR: Mitrovich, V. P.

TITLE: A New Form of Application of the Škoda-Savin Machine for Friction- and Wear Tests With Plastic Materials

PERIODICAL: Zavodskaya laboratoriya, 1960, Vol. 26, No. 12, pp. 1408-1411

TEXT: The Škoda-Savin machine is frequently used for determining the wearability of metal surfaces under special test conditions, the range of use of this machine being limited by the fact that measurement of frictional force is impossible. An additional device to this machine, in which the principal technical characteristics are maintained, makes it possible to use the machine both for determining the wearability and also the coefficients of friction during tests according to the scheme "wave - partial inlet" of various metallic- and non-metallic materials. The same load system was used as in the machine "P" ("R") by M. M. Khrushchev. The reconstructed operating part of the machine is shown in Fig. 1. By way of example, Fig. 2 shows the results obtained by friction- and wear tests of capron, which were carried out without lubrication. The friction area

Card 1/3

MITROVICH, A.N.

Chronic nephritis without hypertension. Sovet. med.
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